

Validation of INNWIND.EU Scaled Model Tests of a Semisubmersible Floating Wind Turbine

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Dipl.-Ing. Friedemann Borisade (né Beyer)
M.Sc. Christian Koch, Dipl.- Ing. Frank Lemmer,
Dipl.-Ing. Denis Matha, Prof. Dr. Po Wen Cheng





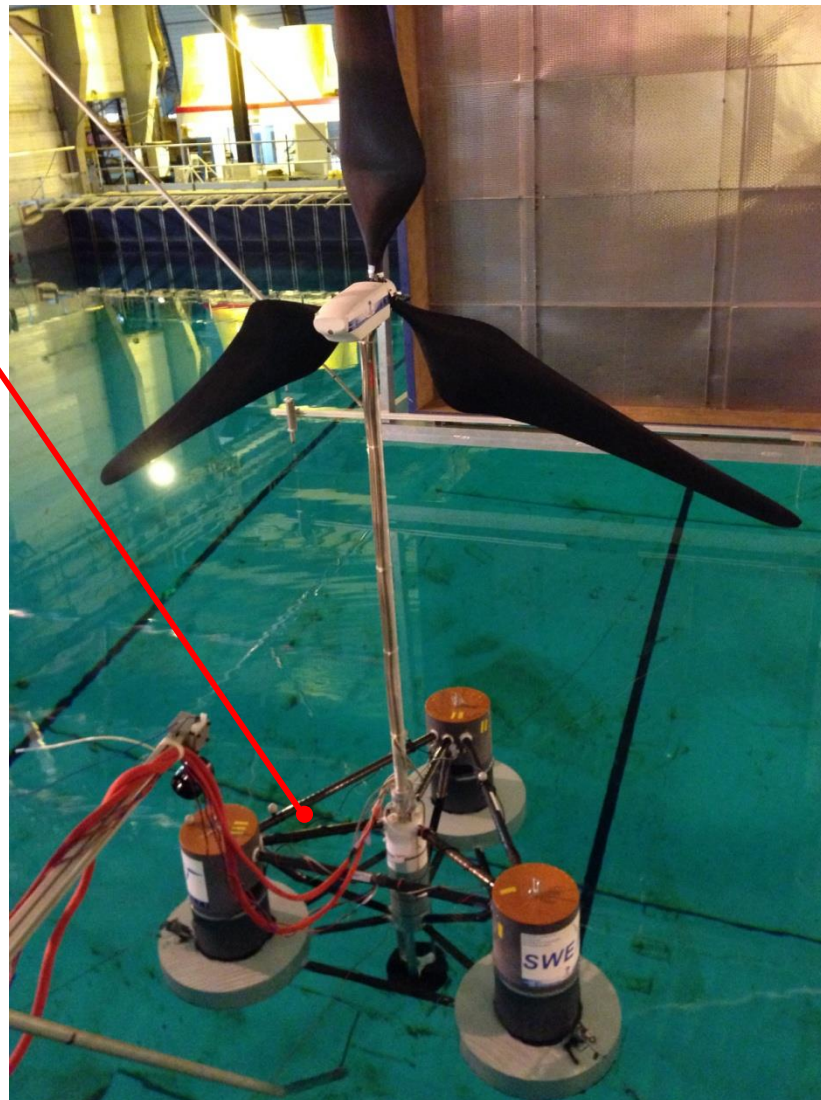
Motivation and Background



Test Campaign:

- 4 weeks in September – November 2014
- combined wind-wave tank LHEEA at École Centrale de Nantes (F)
- **1/60 Froude-scaled** Innwind 10 MW wind turbine (built by POLIMI)
- low-Reynolds Froude-scaled blades
- **semi-submersible** floater based on „OC4-DeepCwind“ (built by USTUTT)
- additional ballast below the floater to achieve scaled CM
- several measuring sensors
- **goals:**
 - increasing experience w/ model tests
 - reducing uncertainty in results
 - deliver another semi-sub dataset

[Florian Amann, SWE]



[Florian Amann, SWE]

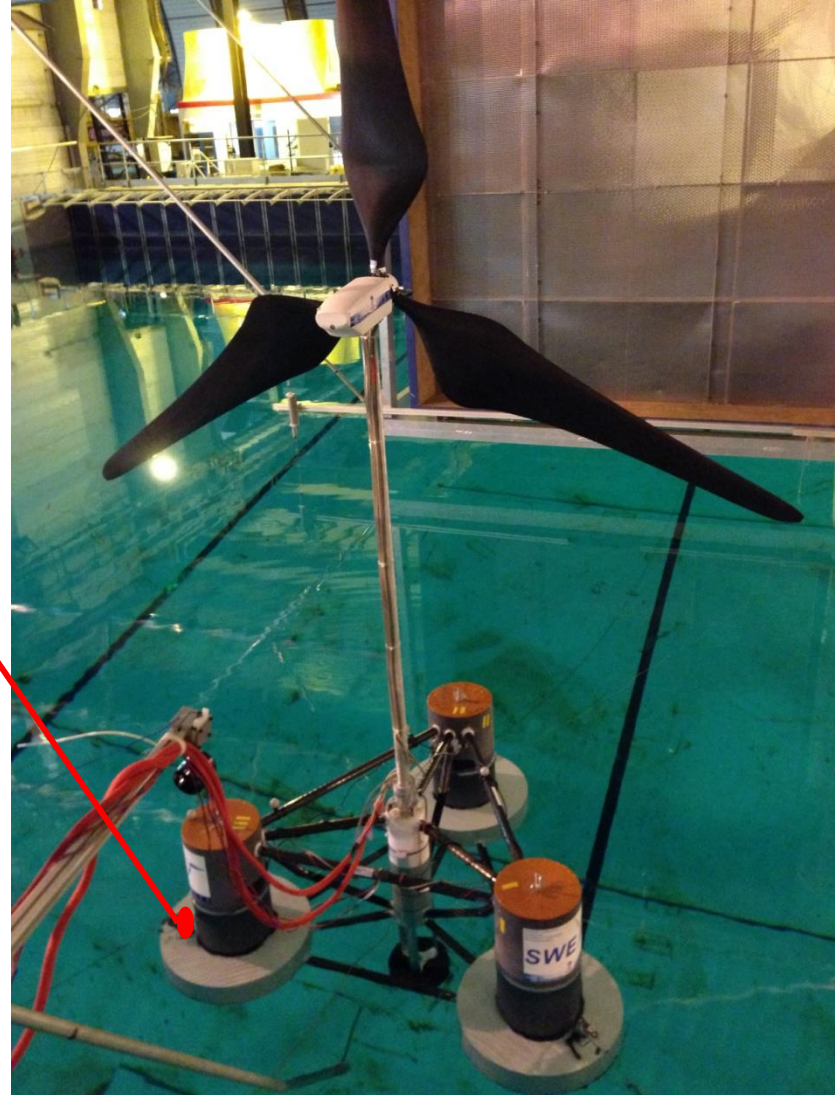
- optical motion tracking system and inertial measuring unit (backup)
- floater surge, sway, heave, roll, pitch, yaw
- accuracy:
1,2 mm / ~0,08 deg

Sensors: Mooring Lines

[Florian Amann, SWE]

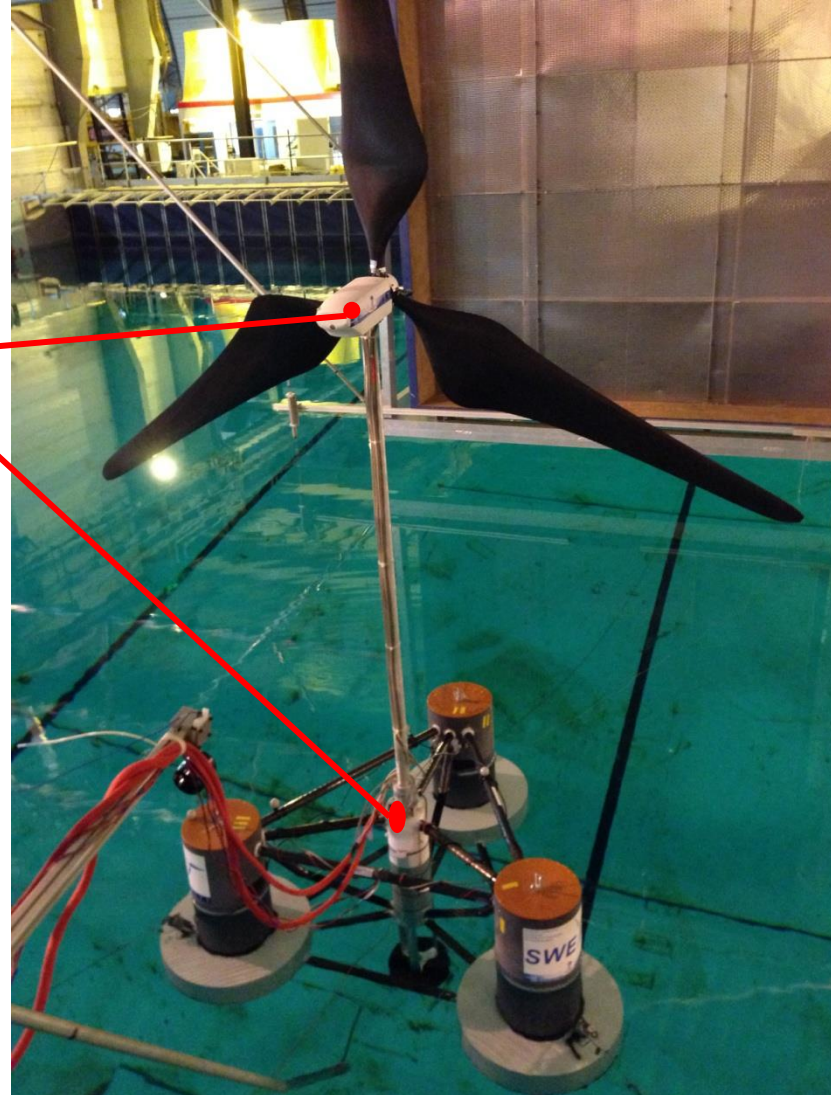


- beam cell with lugs
- vertical fairlead tensions

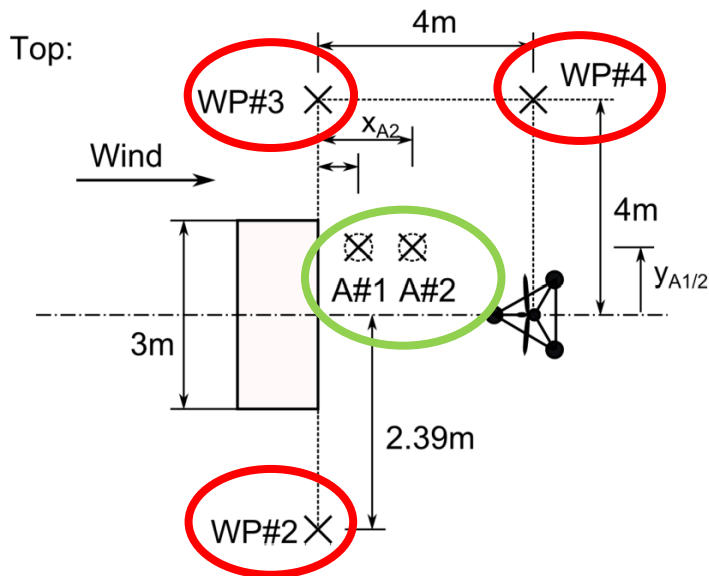


[Florian Amann, SWE]

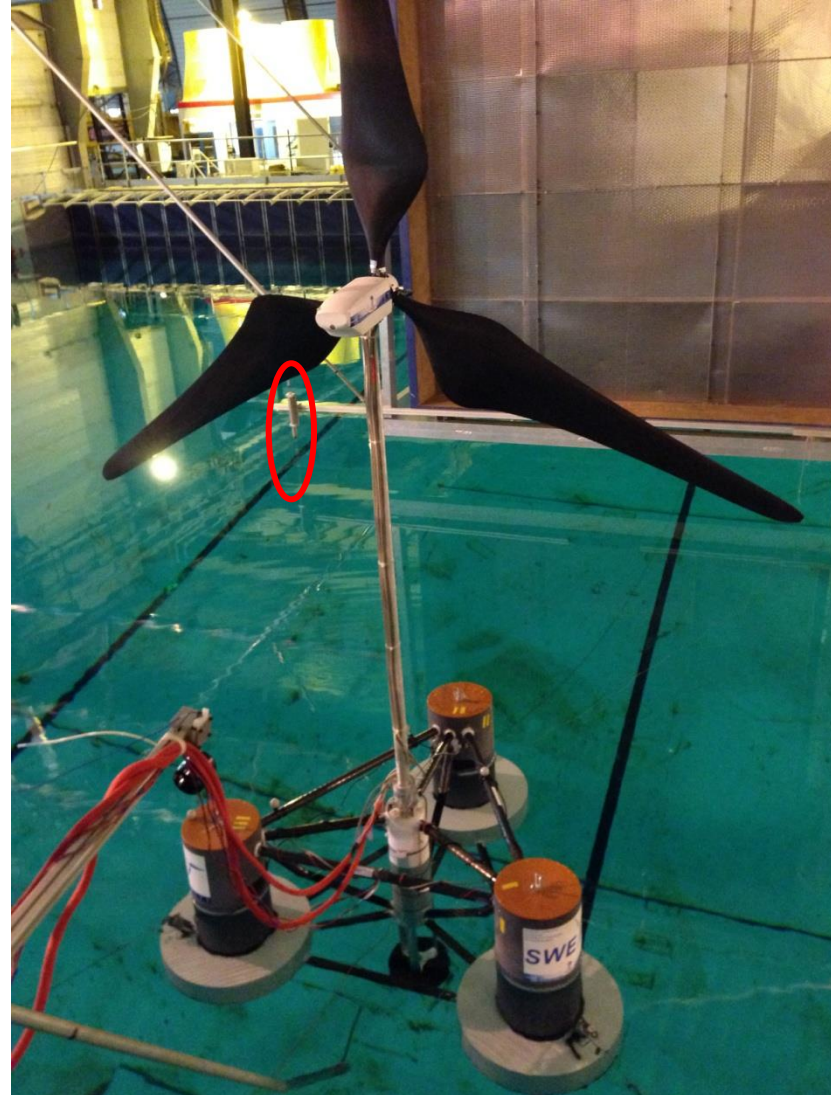
- multiple more sensors
- blade pitch angle
- rotor speed
- power
- shaft bending moment
- generator torque
- rotor azimuth angle
- tower base fore-aft/side-side bending moment



[Florian Amann, SWE]



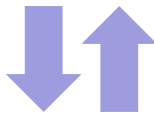
- two **anemometers** and three **wave gauges**
- wave height, wind speed
- signal noise reduction using a Butterworth low-pass filter



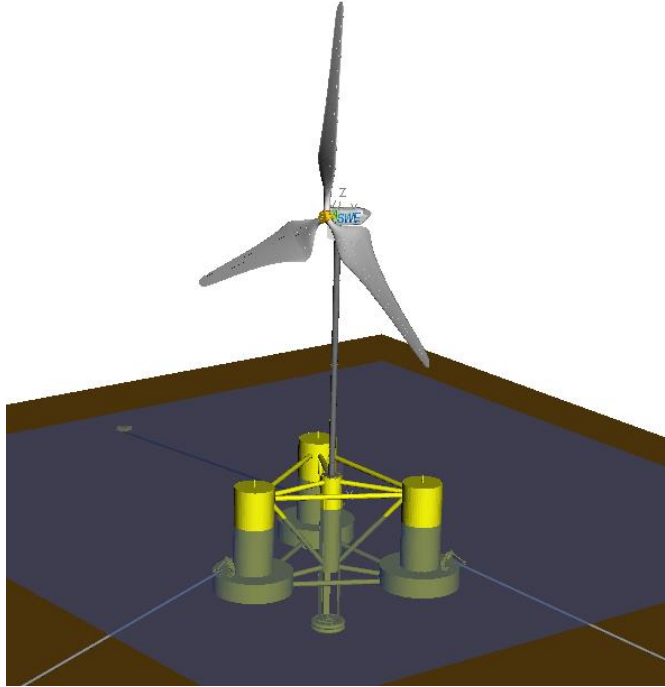



Simulation Model

Aerodynamics
AeroDyn v13.00



Structural Dynamics
Simpack 9.9.1



[Friedemann Borisade, SWE]



Hydrodynamics
HydroDyn v2.02.a-gjh



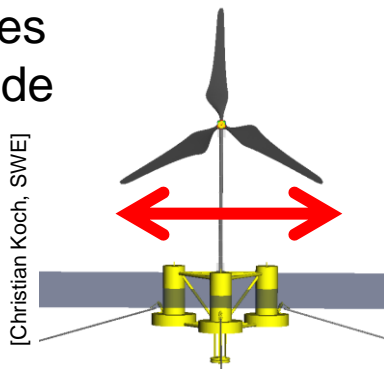
Mooring Dynamics
MAP++ v1.10.0.rc



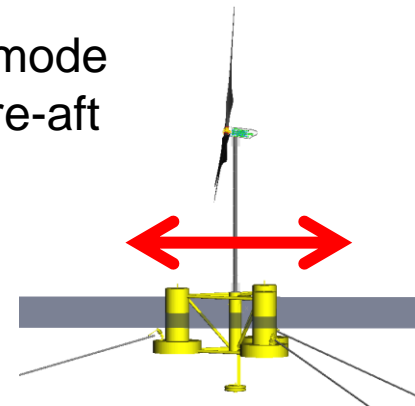
Structural Dynamics

- blades approximated as rigid bodies
- tower modelled as flexible bodies using Timoshenko beams

2 modes
side-side

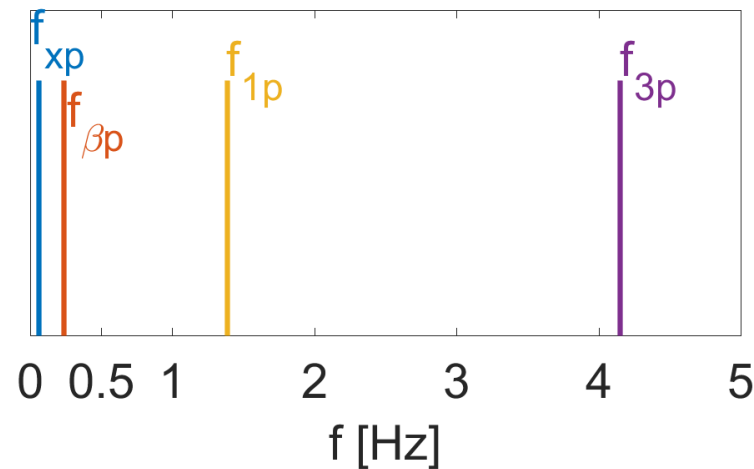


2 mode
fore-aft



Range of
0- 20Hz

- natural frequencies:

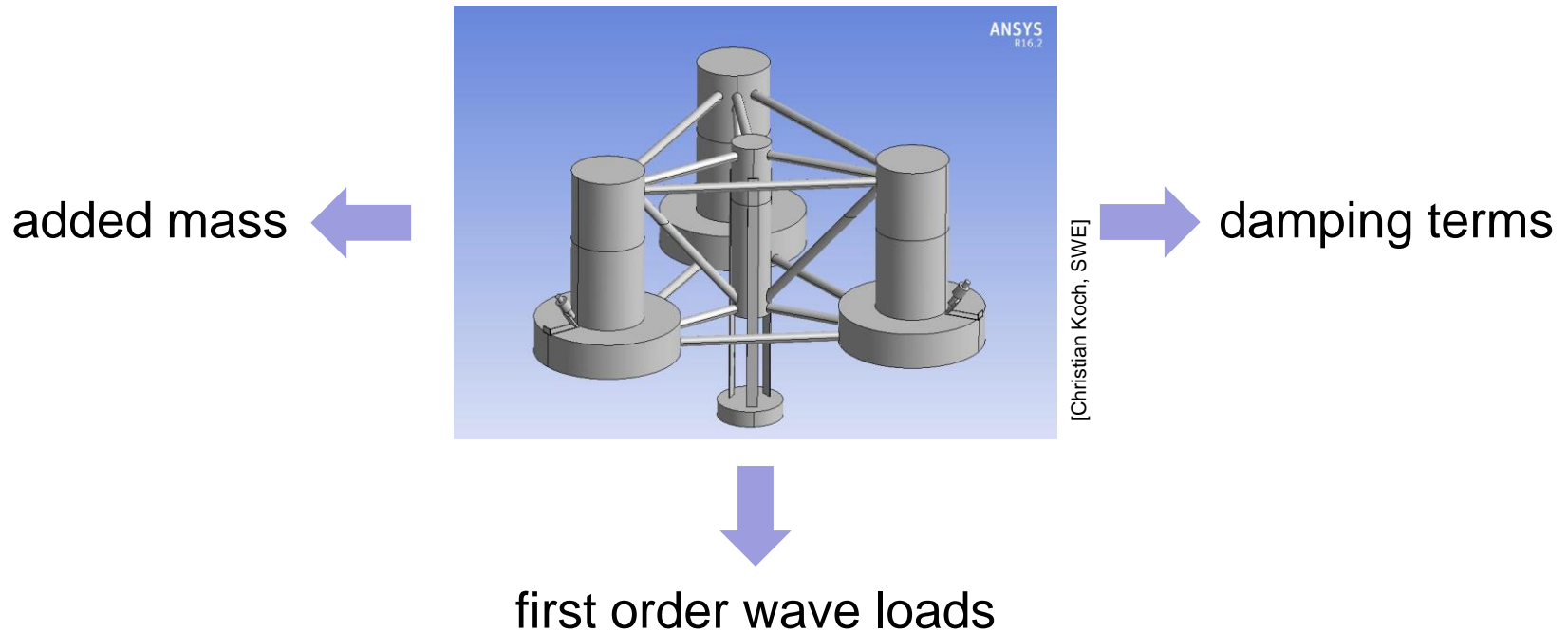


- good agreement between model test and simulation



Hydrodynamics

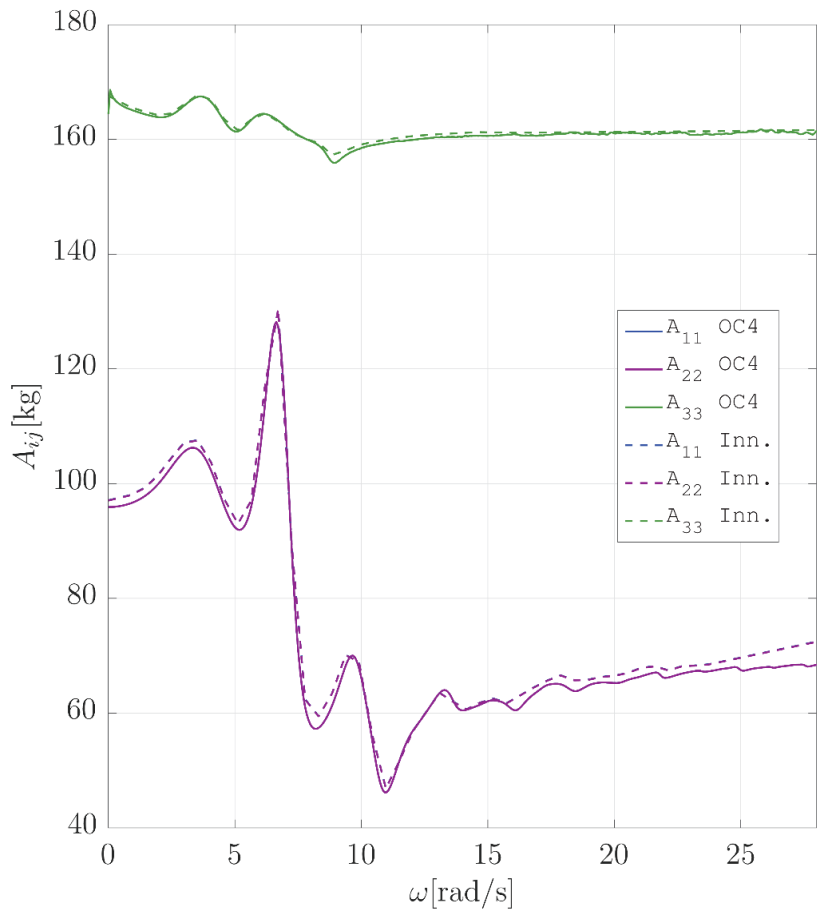
- frequency domain:
 - recalculation of the floater hydrodynamics due to changed hull shape using the panel code software ANSYS AQWA



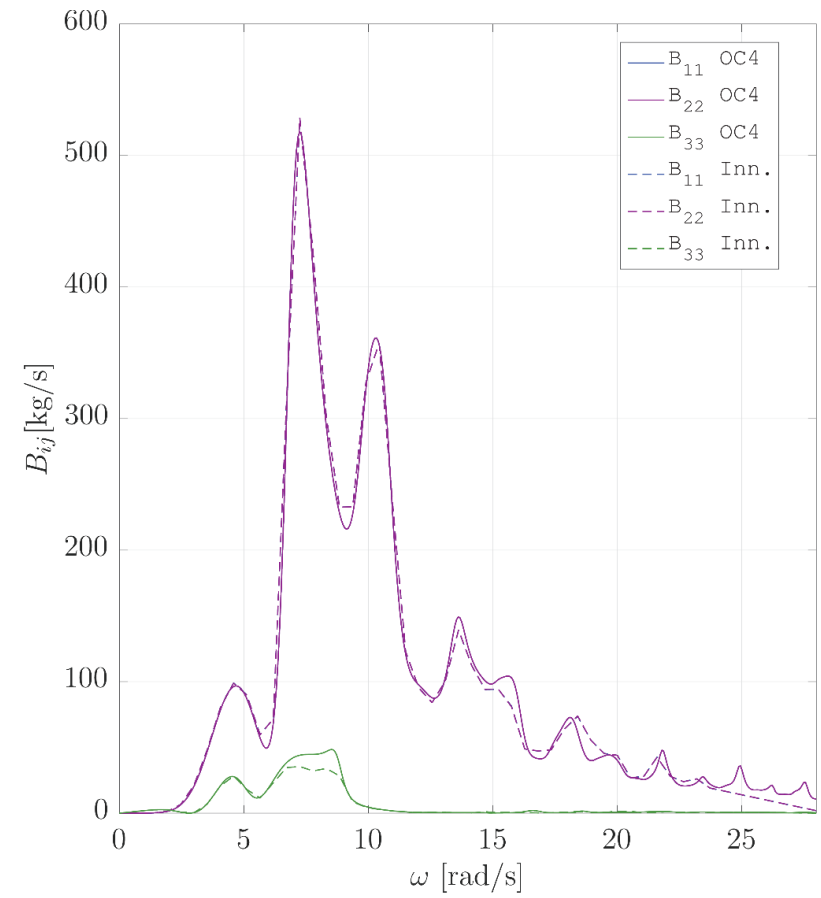
- time Domain (HydroDyn):
 - consideration of member-based Morison elements and second order terms

Added Mass and Damping Coefficients

added mass



damping

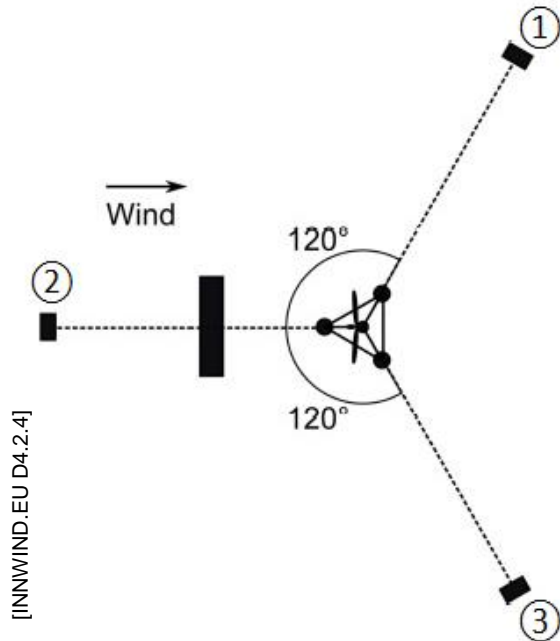


➤ only slight changes between original OC4 and INNWIND.EU



Mooring Dynamics

- quasi-static mooring line model MAP++

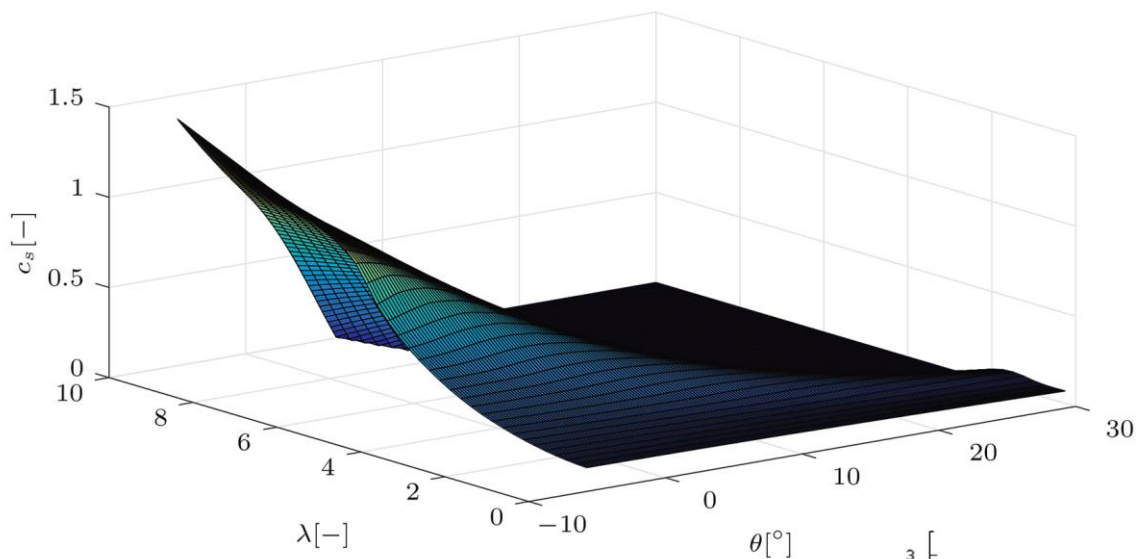


	Fairlead 1			
	Measurement [N]	Sim. [N]	Deviation [%]	Deviation [N]
Displacement 1	9,333	9,845	5,488	0,512
Displacement 2	8,492	8,904	4,849	0,412
Displacement 3	8,246	8,565	3,866	0,319
Displacement 4	8,155	8,434	3,428	0,280
			+4,408	+0,381

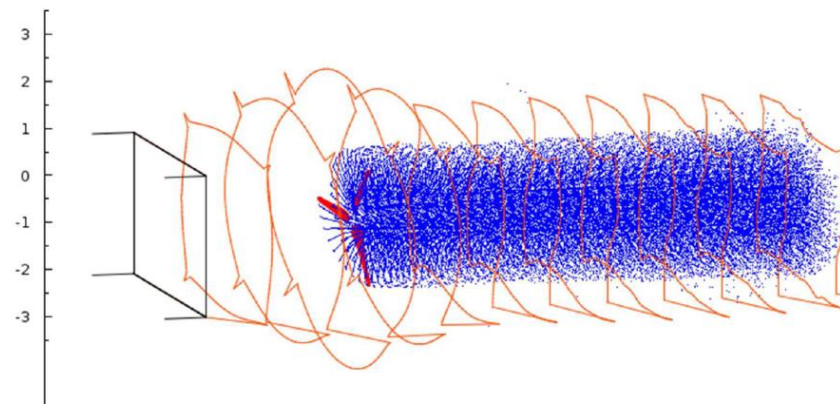
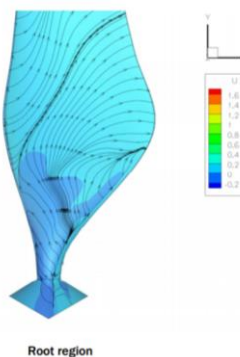
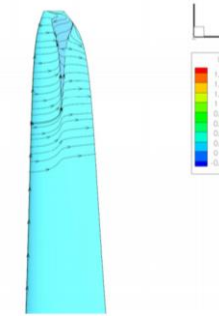
- high sensitivity to axial mooring line stiffness
- high sensitivity to changes; especially regarding to anchor position
- shifting of the radial anchor distance of 0,35 % leads to a mean overall mooring line tension change of nearly 7 %
 - MAP++ shows reasonable results

SWE Aerodynamics

- blade element momentum theory with Prandtl hub- and tip loss model
- no dynamic stall model

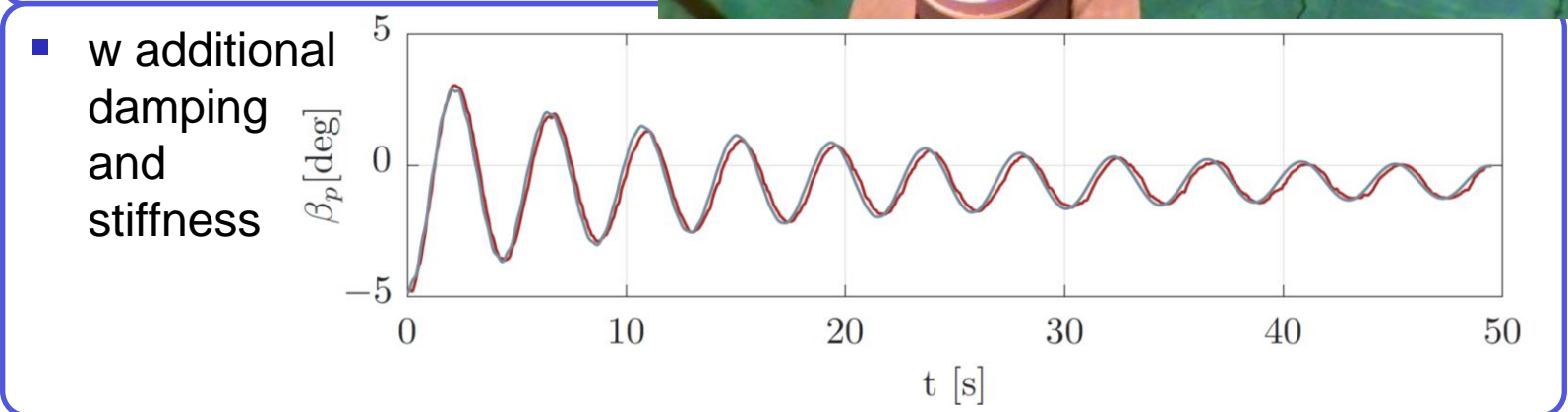
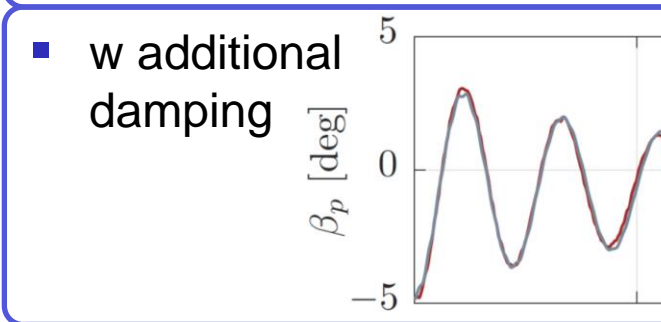
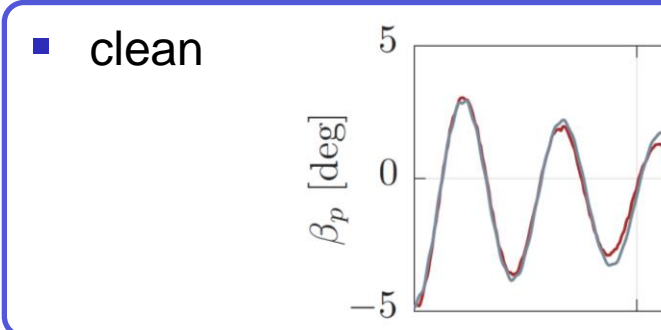


- expanding jet flow



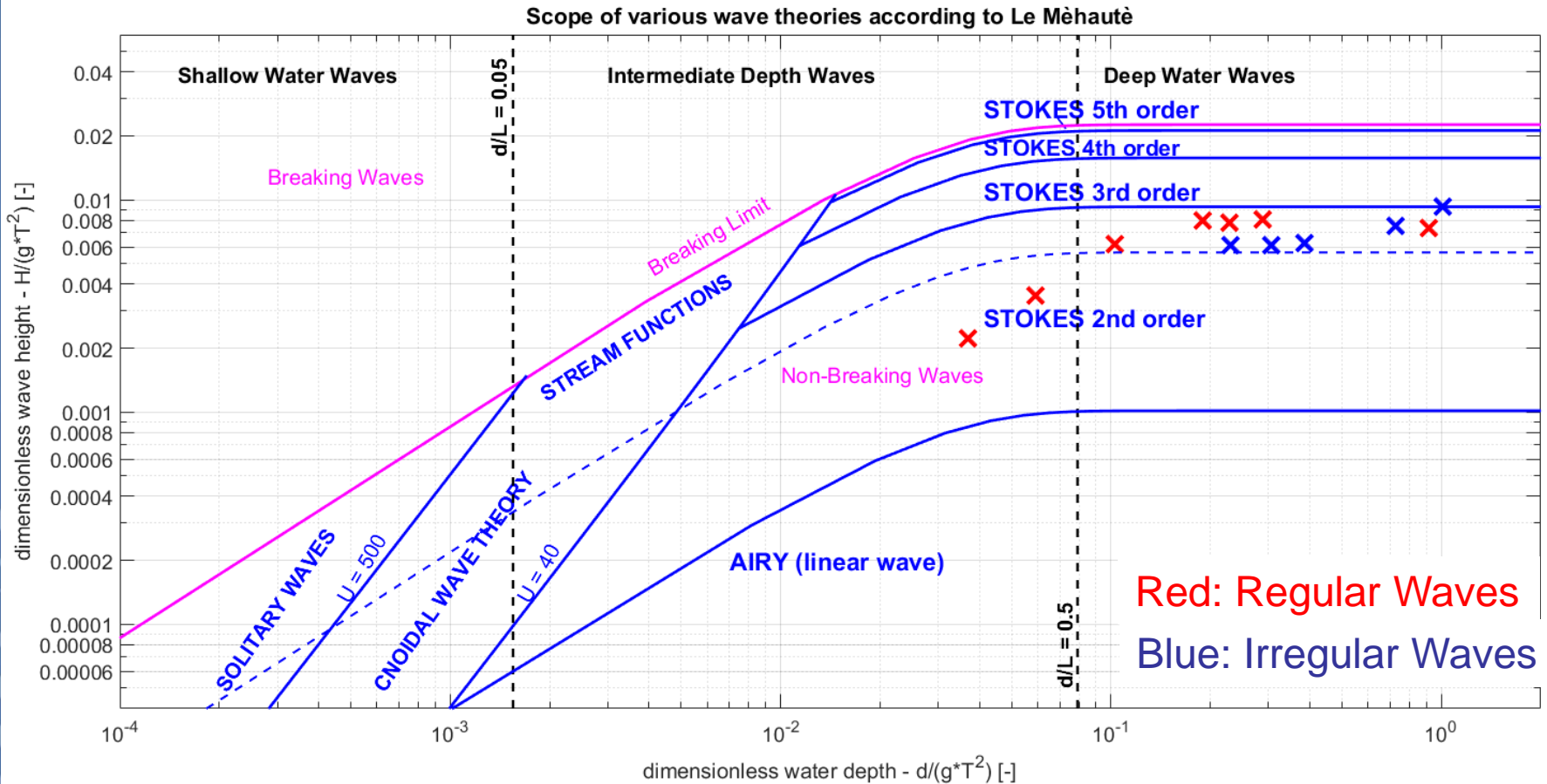
Pitch Free Decay Tests

— measurement
— simulation



➤ good agreement of the hydrodynamic properties

SWE Wave Only Load Cases



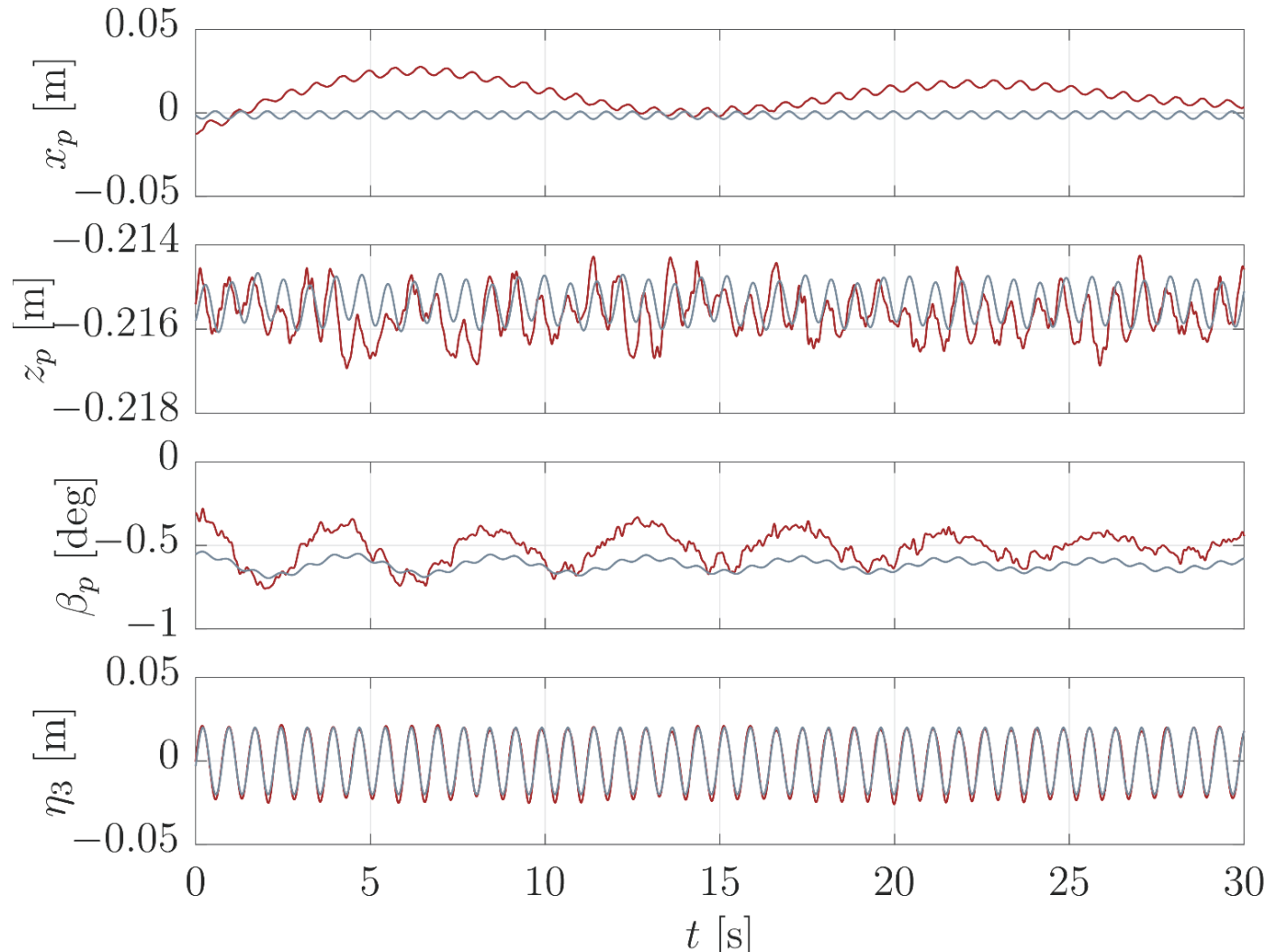
[according to Le Méhauté (1976)]

➤ higher wave theories should be considered

Wave Only: Regular Waves

— measurement
— simulation

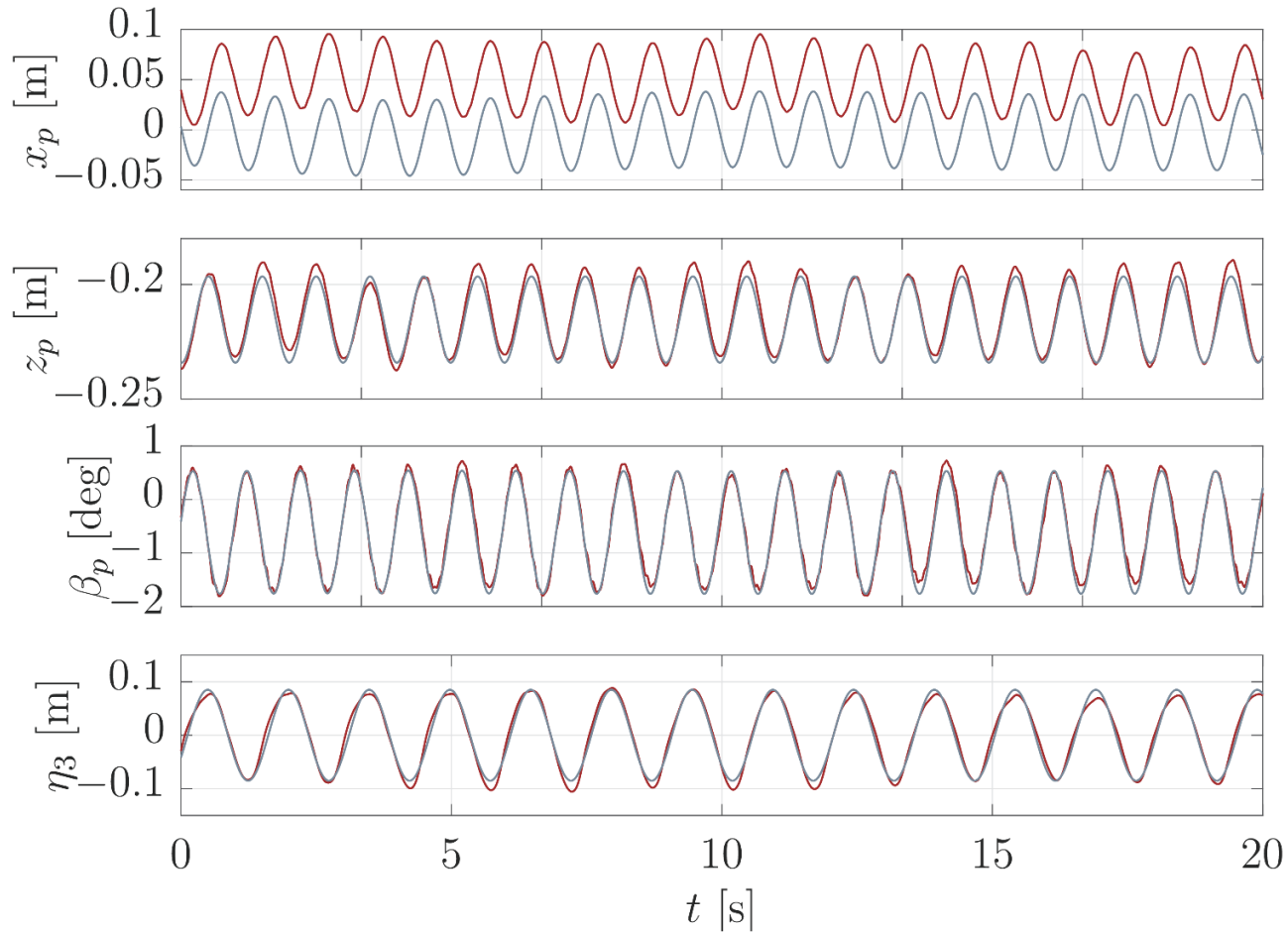
- $H = 0,04$ m; $T_p = 0,746$ s



Wave Only: Regular Waves

— measurement
— simulation

- $H = 0,17$ m; $T_p = 1,493$ s

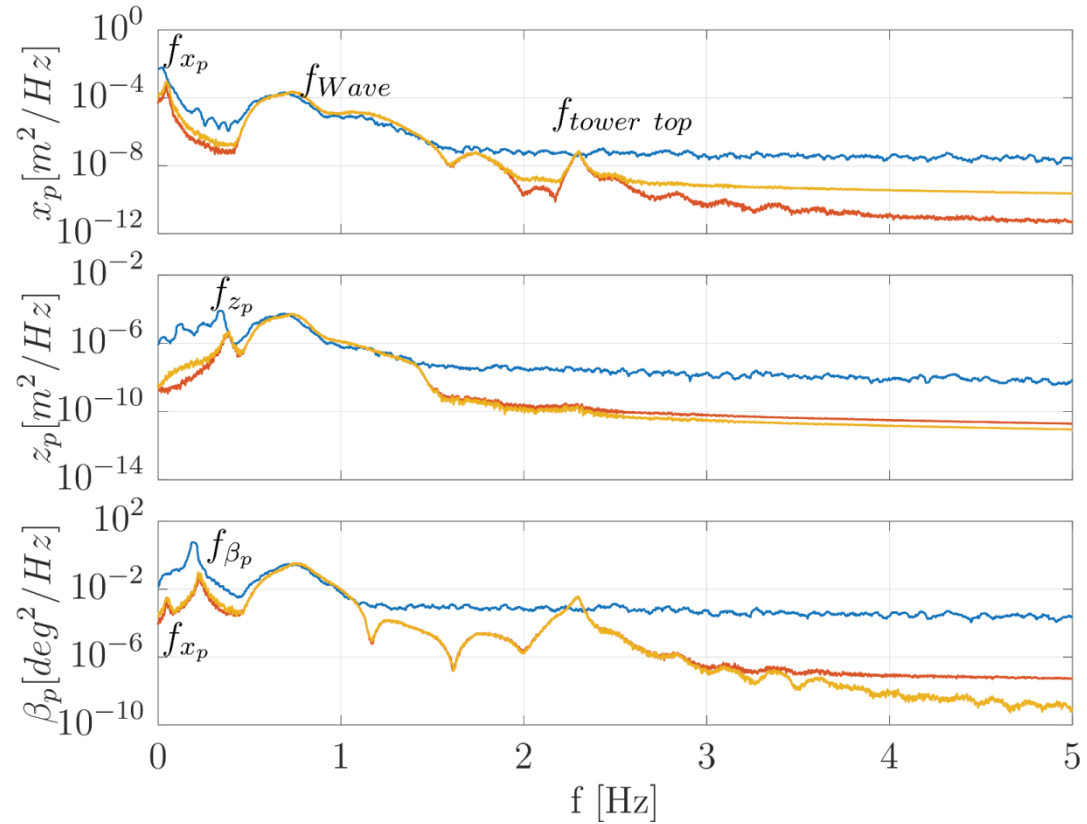
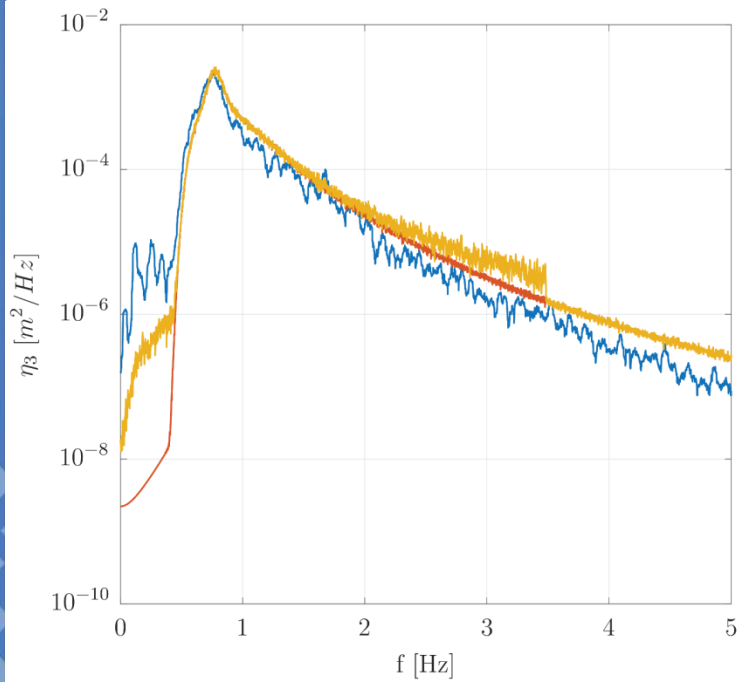


➤ better agreements for larger waves

Wave Only: Irregular Waves

- $H = 0,1 \text{ m}; T_p = 1,291 \text{ s}; \gamma = 2,87$

— measurement
 — simulation 1st
 — simulation 2nd





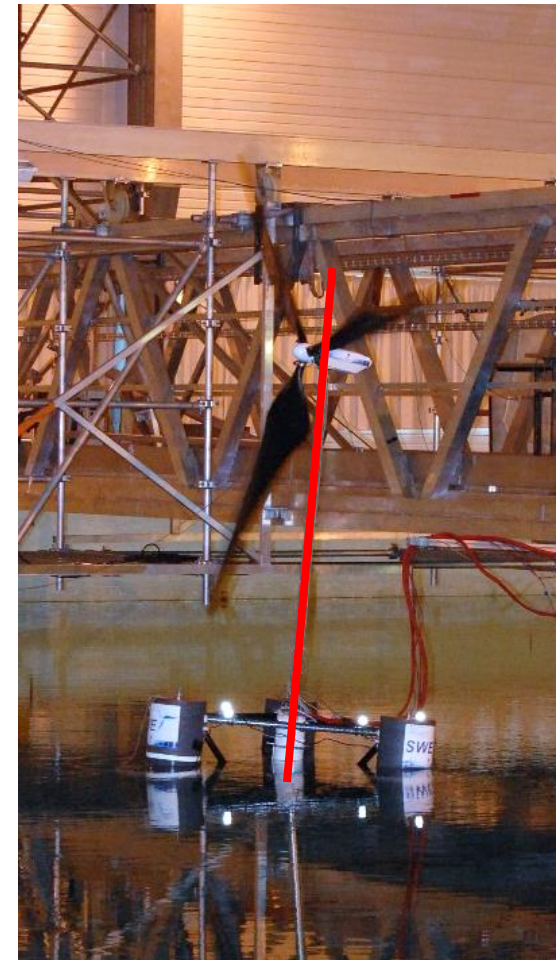
Wind Only

- uncertainties in the wind generation system
- wind speed variations

- surge displacement:

v [m/s]	Exp [m]	Sim [m]	Δ_{abs} [m]	Δ_{rel} [%]
1,50	0,198	0,226	0,03	12,25
1,40	0,198	0,206	0,01	3,69
2,63	0,054	0,090	0,04	40,23
2,58	0,054	0,054	0,00	0,36

- variations of blade pitch angle conducted
 - reduction of wind speed leads to better results

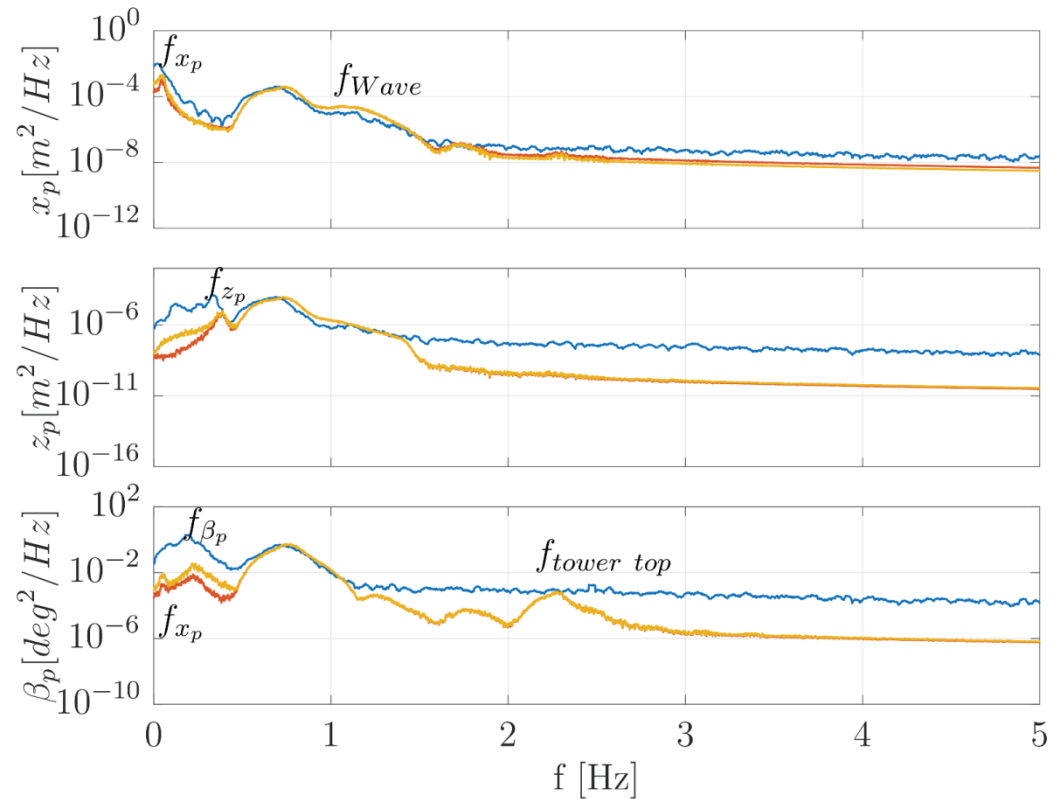
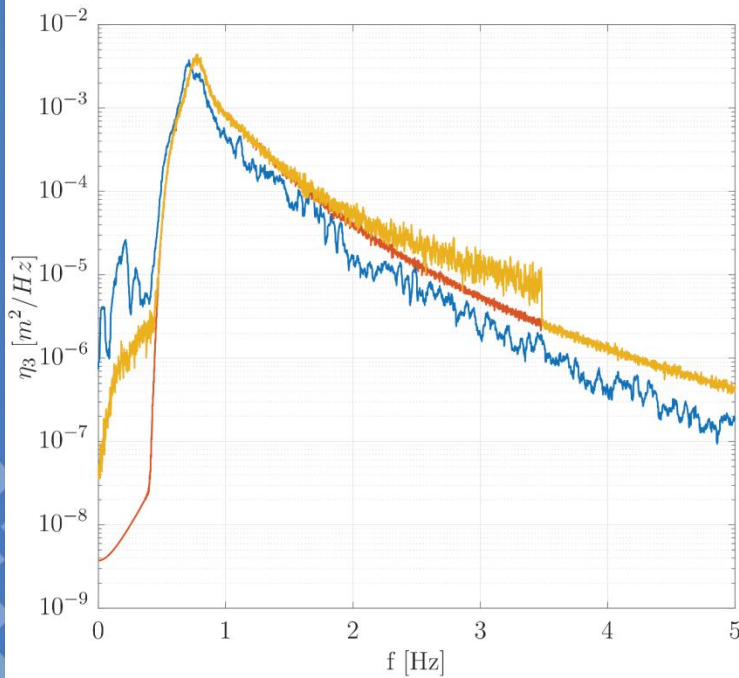


[Henrik Bredmose, DTU]

Wind and Waves: Irregular Wave

— measurement
— simulation 1st
— simulation 2nd

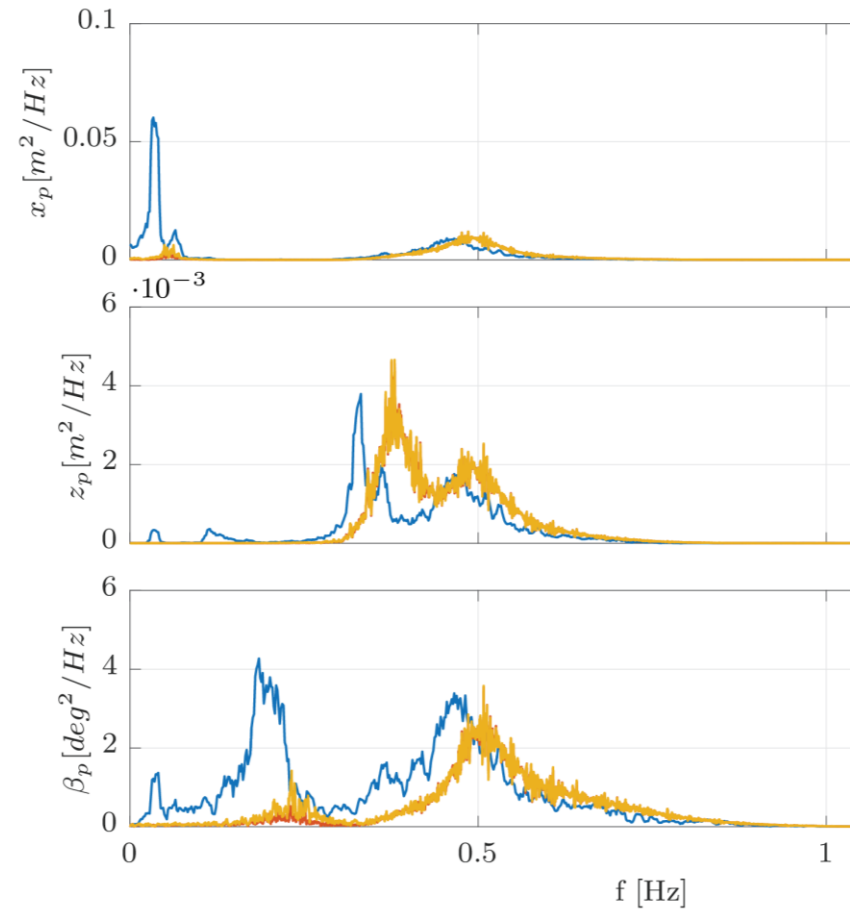
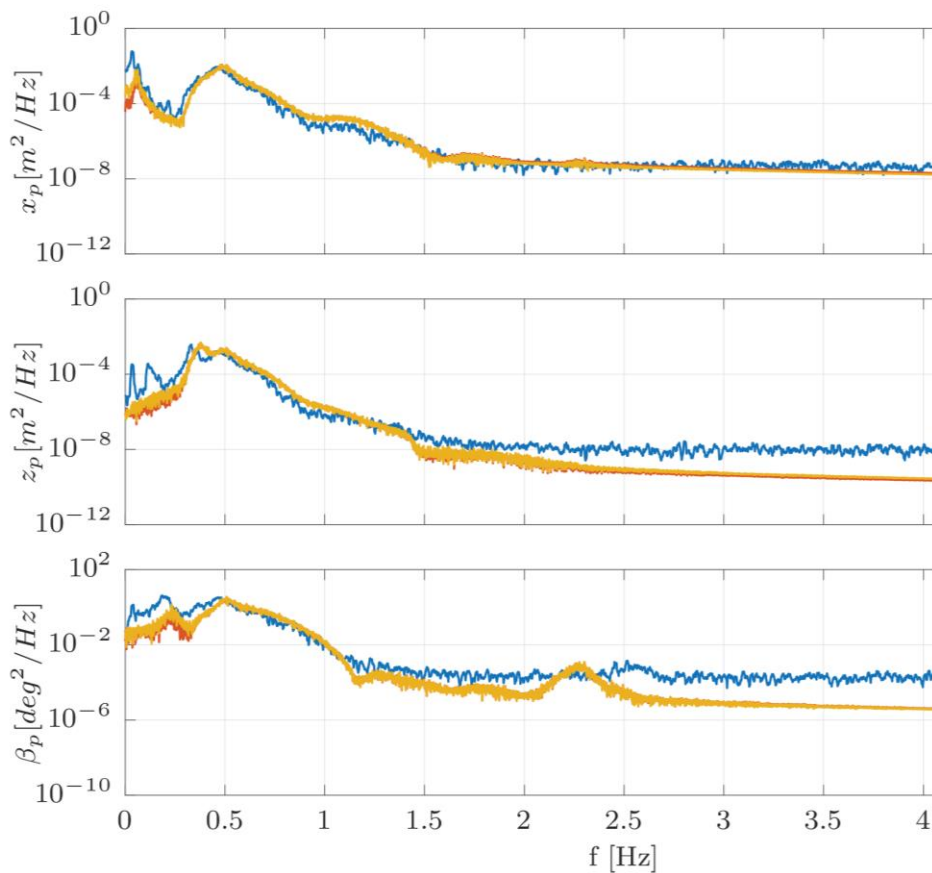
- $v = 2,63 \text{ m/s}$; $H = 0,13 \text{ m}$; $T_p = 1,29 \text{ s}$; $\gamma = 2,87$



Extreme Load Case: Wind and Irregular Waves

- $v = 4 \text{ m/s}$; $H = 0,23 \text{ m}$; $T_p = 2 \text{ s}$; $\gamma = 2,87$

— measurement
 — simulation 1st
 — simulation 2nd



➤ good agreement, missing second order loads in simulation



Summary

- good agreements
 - but: For smaller wave heights the agreements decreases (measuring accuracy, wall friction- and water wave reflections in the tank)
 - MAP++ is showing reasonable results
 - higher order wave theories are required for simulation (slow drift)
 - wind speed and expanding jet flow
-
- successful validation of the simulation model and approach
 - many load cases available that may be used for validation studies



SWE Outlook

- comparison of the results of different simulation codes (D4.25)
 - direct calculation of the QTF matrices in a panel code software
 - conduct model tests with variable blade pitch controller
 - conduct model tests with turbulent wind fields
- Triple Spar Project



Triple Spar Project (1/2)

- April 2016 @ DHI, Denmark
- Participants: CENER, DTU, USTUTT
- Model: DTU 10 MW reference wind turbine mounted to SWE Triple Spar



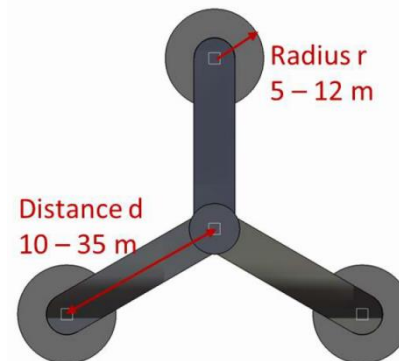
[Henrik Bredmose, DTU]



Triple Spar Project (2/2)



- **community-based public development** including specification report and FAST v8:
 „F. Lemmer et al., *Definition of the SWE-TripleSpar Floating Platform for the DTU 10MW Reference Wind Turbine*, to be published soon online”
- **specified properties:**
 - modified tower properties
 - floater structural properties
 - floater hydrostatic and hydrodynamic properties
 - mooring system
 - control system





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Thank you for your attention!

Dipl.-Ing. **Friedemann Borisade**

Stuttgarter Lehrstuhl für Windenergie (SWE)
Universität Stuttgart
Allmandring 5B - D-70569 Stuttgart, Germany

T: +49 (0) 711 / 685 - 60338

F: +49 (0) 711 / 685 - 68293

E: **borisade@ifb.uni-stuttgart.de**

<http://www.uni-stuttgart.de/windenergie>

<http://www.windfors.de>

